# **Systems Analysis and Control**

Matthew M. Peet Arizona State University

Lecture 19: Drawing Bode Plots, Part 1

## Overview

In this Lecture, you will learn:

## **Drawing Bode Plots**

Drawing Rules

## Simple Plots

- Constants
- Real Zeros

## Review

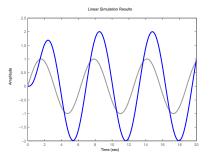
Recall from last lecture: Frequency Response

## Input:

$$u(t) = M\sin(\omega t + \phi)$$

Output: Magnitude and Phase Shift

$$y(t) = |G(i\omega)|M\sin(\omega t + \phi + \angle G(i\omega))|$$



Frequency Response to  $\sin \omega t$  is given by  $G(\imath \omega)$ 

We know  $G(i\omega)$  determines the frequency response.

How to plot this information?

- 1 independent Variable:  $\omega$
- 2 Dependent Variables:  $Re(G(\imath\omega))$  and  $Im(G(\imath\omega))$

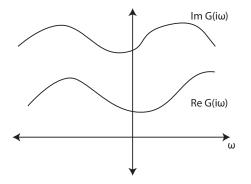


Figure: The Obvious Choice

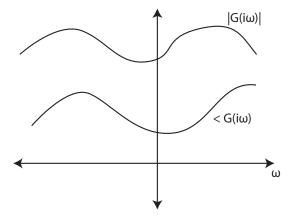
Really 2 plots put together.

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## An Alternative is to plot Polar Variables

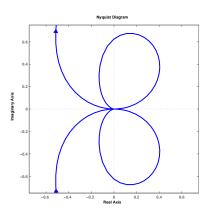
• 1 independent Variable:  $\omega$ 

 $\bullet$  2 Dependent Variables:  $\angle G(\imath \omega)$  and  $|G(\imath \omega)|$ 



- Advantage: All Information corresponds to physical data.
  - ► Can be found directly using a frequency sweep.

If we only want a single plot we can use  $\omega$  as a parameter.



A plot of  $Re(G(\imath\omega))$  vs.  $Im(G(\imath\omega))$  as a function of  $\omega$ .

- Advantage: All Information in a single plot.
- AKA: Nyquist Plot

We focus on Option 2.

### Definition 1.

The Bode Plot is a pair of log-log and semi-log plots:

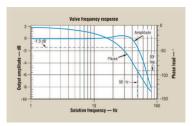
- 1. Magnitude Plot:  $20\log_{10}|G(\imath\omega)|$  vs.  $\log_{10}\omega$
- 2. Phase Plot:  $\angle G(\imath \omega)$  vs.  $\log_{10} \omega$

 $20\log_{10}|G(\imath\omega)|$  is units of **Decibels (dB)** 

- Used in Power and Circuits.
- $10\log_{10}|\cdot|$  in other fields.

Note that by  $\log$ , we mean  $\log$  base 10 ( $\log_{10}$ )

• In Matlab, log means natural logarithm.



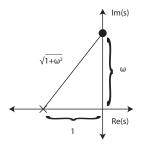
#### Example

Lets do a simple pole

$$G(s) = \frac{1}{s+1}$$

We need

- Magnitude of  $G(\imath \omega)$
- Phase of  $G(\imath \omega)$



Recall that

$$|G(s)| = \frac{|s - z_1| \cdots |s - z_m|}{|s - p_1| \cdots |s - p_n|}$$

So that

$$|G(\imath\omega)| = \frac{1}{|\imath\omega + 1|} = \frac{1}{\sqrt{1 + \omega^2}}$$

#### Example

How to Plot 
$$|G(\imath\omega)| = \frac{1}{\sqrt{1+\omega^2}}$$
?

We actually want to plot it in dB, so ...

$$20\log|G(i\omega)| = 20\log\frac{1}{\sqrt{1+\omega^2}} = 20\log(1+\omega^2)^{-\frac{1}{2}} = -10\log(1+\omega^2)$$

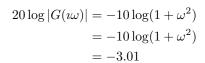
#### Three Cases:

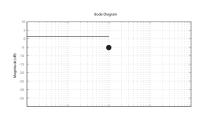
### Case 1: $\omega << 1$

• Approximate  $1 + \omega^2 \cong 1$ 

$$20 \log |G(i\omega)| = -10 \log(1 + \omega^2)$$
  
$$\approx -10 \log 1 = 0$$

Case 2:  $\omega = 1$ 



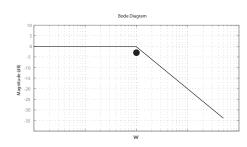


#### Example

### Case 3: $\omega >> 1$

• Approximate: 
$$1+\omega^2\cong\omega^2$$
 
$$20\log|G(\imath\omega)|=-10\log(1+\omega^2)$$

$$\cong -10\log\omega^2$$
$$= -20\log\omega$$



But we use a  $\log - \log$  plot.

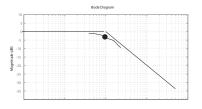
- x-axis is  $x = \log \omega$
- y-axis is  $y = 20 \log |G(i\omega)| = -20 \log \omega = -20x$

**Conclusion:** On the log-log plot, when  $\omega >> 1$ ,

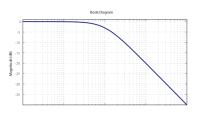
- Plot is Linear
- Slope is -20 dB/Decade!

#### Example

Of course, we need to connect the dots.



## Compare to the Real Thing:



Example: Phase

Now lets do the phase. Recall:

$$\angle G(s) = \sum_{i=1}^{m} \angle (s - z_i) - \sum_{i=1}^{n} \angle (s - p_i)$$

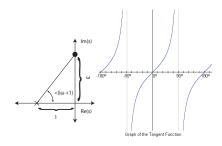
In this case,

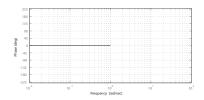
$$\angle G(\imath\omega) = -\angle(\imath\omega + 1)$$
$$= -\tan^{-1}(\omega)$$

Again, 3 cases:

Case 1:  $\omega << 1$ 

- $\tan(\angle G(\imath\omega)) \cong 0$
- $\tan(\angle G(\imath\omega)) \cong \angle G(\imath\omega) \cong 0$





Example: Phase

### Case 2: $\omega = 1$

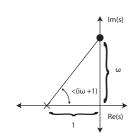
- $tan(\angle G(\imath\omega)) = 1$
- $\angle G(\imath\omega) \cong 45^{\circ}$

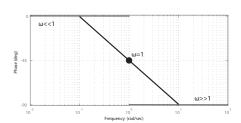
### Between $\omega=.1$ and $\omega=10$ :

- Approximate Slope:
  - $-45^{\circ}/\mathsf{Decade}$

#### Case 3: $\omega >> 1$

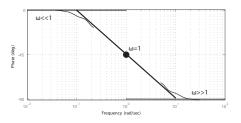
- $\tan(\angle G(\imath\omega)) \cong \frac{1}{0}$
- $\angle G(\imath\omega) \cong -90^{\circ}$
- Fixed at  $-90^{\circ}$  for large  $\omega!$



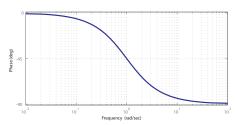


#### Example

We need to connect the dots somehow.



## Compare to the real thing:



#### Methodology

So far, drawing Bode Plots seems pretty intimidating.

- Solving  $tan^{-1}$
- dB and log-plots
- Lots of trig

The process can be Greatly Simplified:

• Use a few simple rules.

Example: Suppose we have

$$G(s) = G_1(s)G_2(s)$$

Then

$$|G(\imath\omega)| = |G_1(\imath\omega)||G_2(\imath\omega)|$$

and

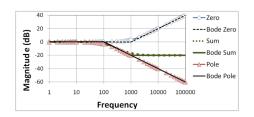
$$\log |G(\imath\omega)| = \log |G_1(\imath\omega)| + \log |G_2(\imath\omega)|$$

Rule # 1

### Rule # 1: Magnitude Plots Add in log-space.

For 
$$G(s) = G_1(s)G_2(s)$$
,

$$20\log|G(\imath\omega)| = 20\log|G_1(\imath\omega)| + 20\log|G_2(\imath\omega)|$$



Decompose G into bite-size chunks:

$$G(s) = \frac{1}{s+3}(s+1)\frac{1}{s^2+3s+1} = G_1(s)G_2(s)G_3(s)$$

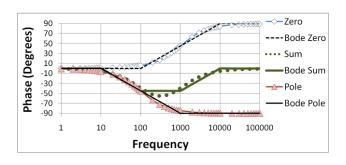
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Rule #2

### Rule # 2: Phase Plots Add.

For 
$$G(s) = G_1(s)G_2(s)$$
,

$$\angle G(\imath\omega) = \angle G_1(\imath\omega) + \angle G_2(\imath\omega)$$



#### Approach

Our Approach is to Decompose G(s) into simpler pieces.

- Plot the phase and magnitude of each component.
- · Add up the plots.

**Step 1:** Decompose G into all its poles and zeros

$$G(s) = \frac{(s - z_1) \cdots (s - z_m)}{(s - p_1) \cdots (s - p_n)}$$

Then for magnitude

$$20 \log |G(\imath\omega)| = \sum_{i} 20 \log |\imath\omega - z_{i}| + \sum_{i} 20 \log \frac{1}{|\imath\omega - p_{i}|}$$
$$= \sum_{i} 20 \log |\imath\omega - z_{i}| - \sum_{i} 20 \log |\imath\omega - p_{i}|$$

And for phase:

$$\angle G(\imath \omega) = \sum_{i} \angle (\imath \omega - z_i) - \sum_{i} \angle (\imath \omega - p_i)$$

But how to plot  $\angle(\imath\omega-z_i)$  and  $20\log|\imath\omega-z_i|$ ?

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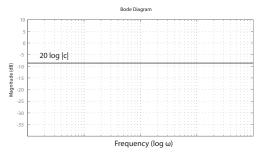
#### The Constant

Before rushing in, lets make sure we don't forget the constant term. If

$$G(s) = c \frac{\left(\frac{s}{z_1} - 1\right) \cdots \left(\frac{s}{z_m} - 1\right)}{\left(\frac{s}{p_1} - 1\right) \cdots \left(\frac{s}{p_n} - 1\right)}$$

Magnitude:  $G_1(s) = c$ 

- $|G_1(\imath\omega)| = |c|$
- $20 \log |G_1(i\omega)| = 20 \log |c|$



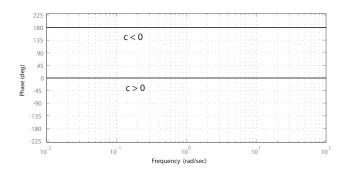
Conclusion: Magnitude is Constant for all  $\omega$ 

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The Constant

**Phase:** 
$$G_1(s) = c$$

$$\angle G_1(\imath\omega) = \angle c = \begin{cases} 0^{\circ} & c > 0\\ 180^{\circ} & c < 0 \end{cases}$$



Conclusion: phase is  $0^{\circ}$  if c > 0, otherwise  $180^{\circ}$ .

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A "Pure" Zero

Lets start with a zero at the origin:  $G_1(s) = s$ .

Magnitude:  $G_1(s) = s$ 

• 
$$|G_1(\imath\omega)| = |\imath\omega| = |\omega|$$

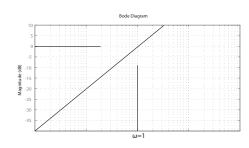
•  $20 \log |G_1(\imath \omega)| = 20 \log |\omega|$ 

Our x-axis is  $\log \omega$ .

- Plot is Linear for all  $\omega$
- Slope is +20 dB/Decade!
- Need a point:  $\omega = 1$

$$20 \log |G_1(i\omega)||_{\omega=1} = 20 \log 1 = 0$$

• Passes through 0 dB at  $\omega = 1$ 



High Gain at High Frequency

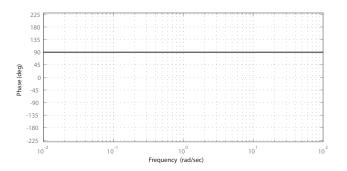
- A pure zero means u'(t)
- The faster the input, The larger the output

A "Pure" Zero: Phase

**Phase:**  $G_1(s) = s$ 

• 
$$\angle G_1(\imath\omega) = \angle \imath\omega = 90^\circ$$

• Always 90°!



Always  $90^{\circ}$  out of phase. Why?

A "Pure" Zero: Multiple Zeros

## What happens if there are multiple pure zeros

• Just what you would expect.

Magnitude: 
$$G_1(s) = s^k$$

• 
$$|G_1(\imath\omega)| = |\imath\omega|^k = |\omega|^k$$

$$20 \log |G_1(i\omega)| = 20 \log |\omega|^k$$
$$= 20k \log |\omega|$$

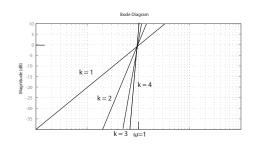
Slope is +20k dB/Decade!

#### Need a Point

• At  $\omega = 1$ :

$$20 \log |G_1(i\omega)||_{\omega=1} = 20k \log 1 = 0$$

• Still Passes through 0dB at  $\omega=1$ 



k pure zeros added together.

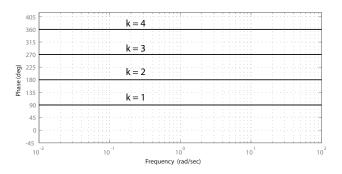
A "Pure" Zero: Multiple Zeros

## And phase for multiple pure zeros?

**Phase:**  $G_1(s) = s^k$ 

• 
$$\angle G_1(\imath\omega) = \angle(\imath\omega)^k = k\angle\imath\omega = 90^\circ k$$

• Always  $90^{\circ}k$ 



k pure zeros added together.

#### Plotting Normal Zeros

A zero at the origin is a line with slope  $+20^{\circ}/\mathrm{Decade}$ .

- What if the zero is not at the origin?
  - We did one example already  $(\frac{1}{s+1})$ .

Change of Format: to simplify steady-state response, we use

$$G_1(s) = (\tau s + 1)$$

- Pole is at  $s=-\frac{1}{\tau}$
- Also put poles in this form

**Rewrite** G(s):  $(s+p) \rightarrow p(\frac{1}{p}s+1)$ .

$$G(s) = k \frac{(s+z_1)\cdots(s+z_m)}{(s+p_1)\cdots(s+p_n)}$$

$$= k \frac{z_1\cdots z_m}{p_1\cdots p_n} \frac{(\frac{1}{z_1}s+1)\cdots(\frac{1}{z_m}s+1)}{(\frac{1}{p_1}s+1)\cdots(\frac{1}{p_n}s+1)}$$

$$= c \frac{(\tau_{z_1}s+1)\cdots(\tau_{z_m}s+1)}{(\tau_{p_1}s+1)\cdots(\tau_{p_n}s+1)}$$

Where

• 
$$au_{zi} = \frac{1}{z_i}$$

• 
$$au_{pi} = \frac{1}{p_i}$$

$$\bullet \ c = k \frac{z_1 \cdots z_m}{p_1 \cdots p_n}$$

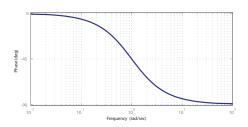
Assume  $z_i$  and  $p_i$  are Real.

Plotting Normal Zeros

$$G(s) = c \frac{(\tau_{z1}s + 1) \cdots (\tau_{zm}s + 1)}{(\tau_{p1}s + 1) \cdots (\tau_{pn}s + 1)}$$

The advantage of this form is that steady-state response to a step is

$$y_{ss} = \lim_{s \to 0} G(s) = G(0) = c$$



Low Frequency Response is given by the constant term, c.

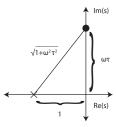
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Plotting Normal Zeros

$$G_1(s) = (\tau s + 1)$$
$$|G_1(i\omega)| = |i\omega\tau + 1| = \sqrt{1 + \tau^2\omega^2}$$

## Magnitude:

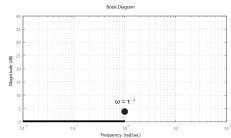
$$20\log|G_1(i\omega)| = 20\log(1+\omega^2\tau^2)^{\frac{1}{2}} = 10\log(1+\omega^2\tau^2)$$



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#### Case 1: $\omega \tau << 1$

- Approximate  $1 + \omega^2 \tau^2 \cong 1$   $20 \log |G(\imath \omega)| = 20 \log(1 + \omega^2 \tau^2)$  $\cong 20 \log 1 = 0$
- Case 2:  $\omega \tau = 1$   $20 \log |G(\imath \omega)| = 10 \log(1 + \omega^2 \tau^2)$  $= 10 \log 2 = 3.01$

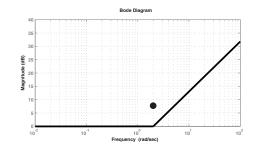


#### Example

### Case 3: $\omega \tau >> 1$

• Approximate 
$$1 + \omega^2 \tau^2 \cong \omega^2 \tau^2$$

$$\begin{aligned} 20 \log |G(\imath \omega)| &= 20 \log \sqrt{1 + \omega^2 \tau^2} \\ &\cong 10 \log \omega^2 \tau^2 \\ &= 20 \log \omega \tau \\ &= 20 \log \omega + 20 \log \tau \end{aligned}$$



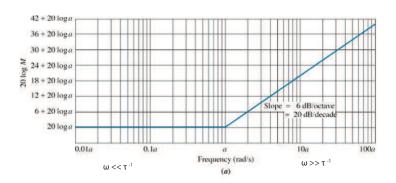
## **Conclusion:** When $\omega \tau >> 1$ .

- Plot is Linear
- Slope is +20 dB/Decade!
- inflection at  $\omega = \frac{1}{\tau}$

#### Plotting Normal Zeros

Compare this to the magnitude plot of

$$G_1(s) = s + a$$



This is why we use the format  $G_1(s) = \tau s + 1$ 

• We want 0dB (no gain) at low frequency.

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## Summary

What have we learned today?

### **Drawing Bode Plots**

• Drawing Rules

### Simple Plots

- Constants
- Real Zeros

Next Lecture: More Bode Plotting