

# Spacecraft Dynamics and Control

Matthew M. Peet

Lecture 8: Impulsive Orbital Maneuvers

# Introduction

In this Lecture, you will learn:

## Coplanar Orbital Maneuvers

- Impulsive Maneuvers
  - ▶  $\Delta v$
- Single Burn Maneuvers
- Hohmann transfers
  - ▶ Elliptic
  - ▶ Circular

**Numerical Problem:** Suppose we are in a circular parking orbit at an altitude of 191.34km and we want to raise our altitude to 35,781km. Describe the required orbital maneuvers (time and  $\Delta v$ ).

# Changing Orbits

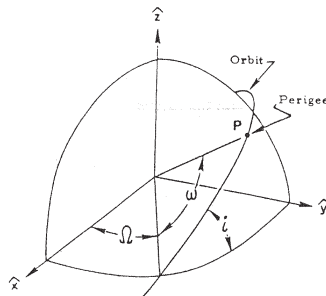
Suppose we have designed our ideal orbit.

- We have chosen  $a_d, e_d, i_d, \Omega_d, \omega_d$
- We are currently in orbit  $a_0, e_0, i_0, \Omega_0, \omega_0$ 
  - ▶ Determined from current position  $\vec{r}$  and velocity  $\vec{v}$ .

## Question:

- How to get from current orbit to desired orbit?
- What tools can we use?
- What are the constraints?

Unchanged, the object will remain in **initial orbit** indefinitely.



# Lecture 8

## Spacecraft Dynamics

### Changing Orbits

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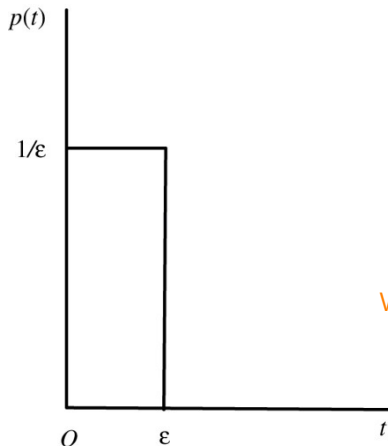
Unchanged, the object will remain in **initial orbit** indefinitely.



- For now, we don't care about  $f$  (time)
  - Lambert's Problem
  - Can correct using phasing
- Don't care about efficiency
- true anomaly ( $f$ ) determines phasing within the orbit and is easily altered post-insertion.

# How to create a $\Delta v$

$\Delta v$  is our tool for changing orbits



The change in position is

Velocity change is caused by thrust.

- For constant thrust,  $F$ ,

$$v(t) = v(0) + \frac{F}{m} \Delta t$$

- for a desired  $\Delta v$ , the time needed is

$$\Delta t = \frac{m \Delta v}{F}$$

We assume  $\Delta t$  and  $\Delta \vec{r}$  are *negligible* for a  $\Delta v$ .

- No continuous thrust transfers
- Although these are increasingly important.

$$\Delta \vec{r}(t) = \frac{m \Delta v^2}{2F}$$

# Lecture 8

## Spacecraft Dynamics

### How to create a $\Delta v$

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$\rho(t)$

$1/F$

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- Although these are increasingly important.

$$\Delta r(t) = \frac{m \Delta v^2}{2F}$$

- For fixed  $\Delta v$ , if  $\frac{m}{F}$  is small, the  $\Delta \vec{r}$  is small
- We will assume  $\Delta \vec{r} = 0$

$$v(t) = v(0) + \frac{F}{m} t$$

so

$$t = \Delta v \frac{m}{F}$$

Now,

$$r(t) = r(0) + v(0)t + \frac{F}{2m} t^2$$

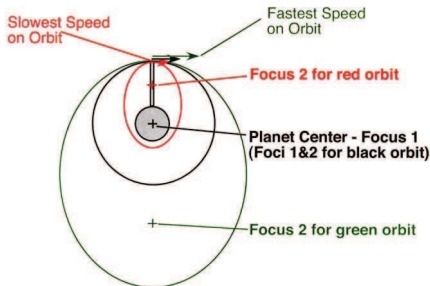
$$\Delta r = v(0)t + \frac{F}{2m} \Delta v^2 \frac{m^2}{F^2}$$

$$= v(0) \Delta v \frac{m}{F} + \frac{\Delta v^2}{2} \frac{m}{F} = \left( v(0) \Delta v + \frac{\Delta v^2}{2} \right) \frac{m}{F}$$

However, we can ignore the  $v(0)$  if we are considering deviation from a nominal path.

# $\Delta V$ moves the vacant focus of the orbit

Orbit maneuvers are made through changes in velocity.



- $\vec{r}$  and  $\vec{v}$  determine orbital elements.
- Our first constraint is *continuity*.
  - ▶ New orbit must also pass through  $\vec{r}$ .
  - ▶ Cannot jump from one orbit to another instantly
  - ▶ If the **initial orbit** and **target orbit** don't intersect, a **transfer orbit** is required.
- Can changes in  $\vec{v}$  alone be used to achieve a desired  $a$ ,  $e$ ,  $i$ ,  $\Omega$ ,  $\omega$  ?

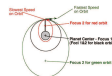
# Lecture 8

## Spacecraft Dynamics

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## Equations involving velocity

$$v_c = \sqrt{\frac{\mu}{r_c}}$$

circular orbit

$$v = \sqrt{\mu \left( \frac{2}{r} - \frac{1}{a} \right)}$$

vis-viva

$$v_p = \sqrt{\frac{\mu}{a} \left( \frac{1+e}{1-e} \right)}$$

periapse velocity

$$v_a = \sqrt{\frac{\mu}{a} \left( \frac{1-e}{1+e} \right)}$$

apoapse velocity

$$v_{esc} = \sqrt{\frac{2\mu}{r}}$$

escape velocity

$$\vec{v} = \begin{bmatrix} -\frac{\mu}{h} (\cos \Omega (\sin(\omega + f) + e \sin \omega) + \sin \Omega (\cos(\omega + f) + e \cos \omega) \cos i) \\ -\frac{\mu}{h} (\sin \Omega (\sin(\omega + f) + e \sin \omega) - \cos \Omega (\cos(\omega + f) + e \cos \omega) \cos i) \\ \frac{\mu}{h} (\cos(\omega + f) + e \cos \omega) \sin i \end{bmatrix}$$



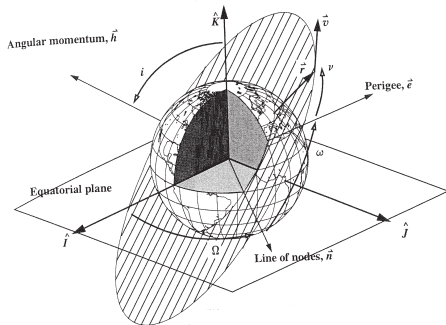
# What can we do with a $\Delta v$ Maneuver?

$\Delta v$  refers to the difference between the initial and final velocity vectors.

A  $\Delta v$  maneuver can:

- Raise/lower the apogee/perigee
- A change in inclination
- Escape
- Reduction/Increase in period
- Change in RAAN
- Begin a 2+ maneuver sequence of burns.

► Creates a **Transfer Orbit**.



We'll start by talking about coplanar maneuvers.

# Lecture 8

## Spacecraft Dynamics

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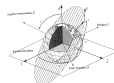
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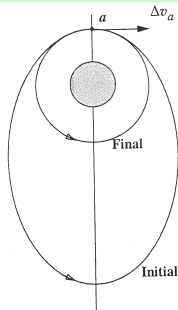
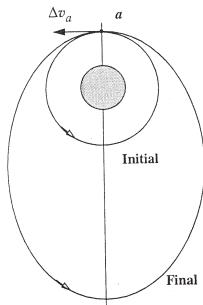
- Raise/lower the apogee/perigee is performed at perigee/apogee
- A change in inclination is *usually* performed at the equatorial plane (any inclination achievable from this point).
- Small changes in period help with phase changes  $f(t)$ .
- Change in RAAN should be done as far from equatorial plane as possible.

# Single Burn Coplanar Maneuvers

Apogee or Perigee raising or lowering.

## Definition 1.

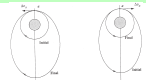
**Coplanar Maneuvers** are those which do not alter  $i$  or  $\Omega$ .



- Only  $a$  and  $e$  change
- for fixed  $r$ :  $v$  allows us to control  $a$

$$v = \sqrt{\mu \left( \frac{2}{r} - \frac{1}{a} \right)}$$

vis-viva

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vis-viva

**Concept: Tangential Burns**

- For maximum efficiency, a burn must occur at  $0^\circ$  flight path angle
- Tangential burns can occur at perigee and apogee

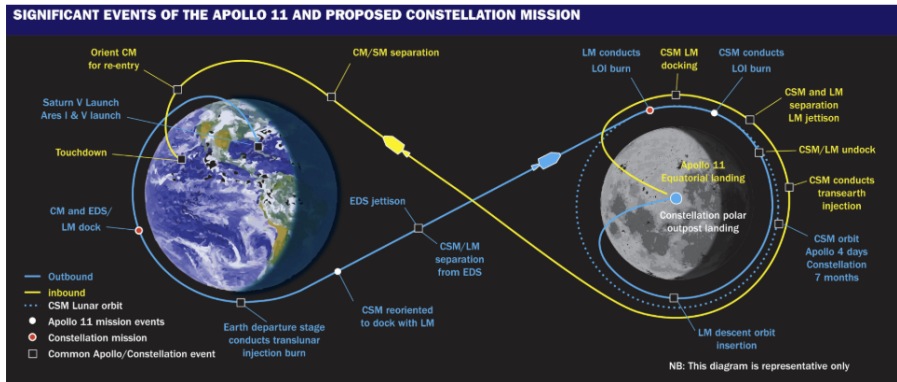
We will explain why we want  $\angle FPA = 0^\circ$  in Lecture 9, when we discuss the Oberth effect.

# The First Burn: Insertion into a Parking Orbit

A perigee raising maneuver

Suppose we launch from the surface of the earth.

- This creates an initial elliptic orbit which will re-enter.
- To circularize the orbit, we plan on using a burn at apogee.



**Problem:** We are given  $a$  and  $e$  of the initial elliptic orbit. Calculate the  $\Delta v$  required at apogee to circularize the orbit.

# Example: Insertion into a Parking Orbit

The First  $\Delta v$  burn: A perigee raising maneuver

**Calculating the  $\Delta v$ :** To raise the perigee, we burn tangentially at apogee. At apogee, we have that

$$r_{a_0} = a_0(1 + e_0)$$

From the vis-viva equation, we can calculate the velocity at apogee.

$$v_{a_0} = \sqrt{\mu \left( \frac{2}{r_{a_0}} - \frac{1}{a_0} \right)} = \sqrt{\frac{\mu}{a_0} \left( \frac{1 - e_0}{1 + e_0} \right)}$$

Our **target orbit** is circular with radius  $r_d = a_d = r_{a_0}$ . The velocity of the target orbit is constant at

$$v_c = \sqrt{\frac{\mu}{r_a}} = \sqrt{\frac{\mu}{a(1 + e)}}$$

Therefore, the  $\Delta v$  required to circularize the orbit is

$$\Delta v = v_c - v_{a_0} = \sqrt{\frac{\mu}{a_0(1 + e_0)}} - \sqrt{\frac{\mu}{a_0} \left( \frac{1 - e_0}{1 + e_0} \right)}$$

- It is unusual to launch directly into the desired orbit. Instead we use the parking orbit while waiting for more complicated orbital maneuvers.



## Lecture 8

## Spacecraft Dynamics

## Concept: Transfer Orbits

## Concept: Transfer Orbits

How to calculate the  $\Delta v$ ?To obtain both desired  $a$  and  $v$ , we need **two** maneuvers.

## Definition 2.

- The **Initial Orbit** is the orbit we want to leave.
- The **Target Orbit** is the orbit we want to achieve.
- The **Transfer Orbit** is an orbit which intersects both the initial orbit and target orbit.

Step 1: Design a **transfer orbit** -  $a, e, i, \omega, \Omega, f$ Step 2: Calculate  $\vec{v}_{tr,1}$  at the point of interaction with initial orbit.Step 3: Calculate initial burn to maneuver into **transfer orbit**.

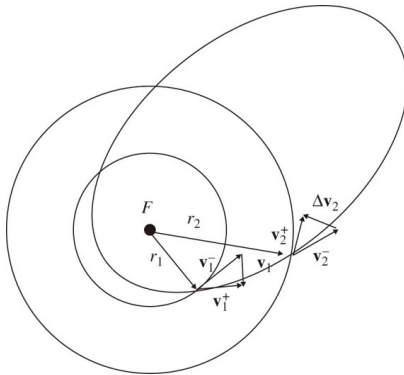
$$\Delta \vec{v}_1 = \vec{v}_{tr,1} - \vec{v}_{init}$$



- Note that in the illustration, the transfer orbit is not a Hohmann transfer, which is the most common type of transfer orbit.
- Step 1 may be **VERY HARD** because you may not know what  $f_{tr}$  will be in your transfer orbit!



# Coplanar Two-Impulse Orbit Transfers



**Step 4:** Calculate  $\vec{v}_{tr,2}$  at the point of intersection with **target orbit**.

**Step 5:** Calculate velocity of the **target orbit**,  $\vec{v}_{fin}$ , at the point of intersection with **transfer orbit**.

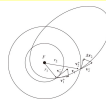
**Step 6:** Calculate the final burn to maneuver into **target orbit**.

$$\Delta v_2 = \vec{v}_{fin} - \vec{v}_{tr,2}$$

# Lecture 8

## Spacecraft Dynamics

### Coplanar Two-Impulse Orbit Transfers



**Step 4:** Calculate  $\vec{r}_{tr,2}$  at the point of intersection with **target orbit**.

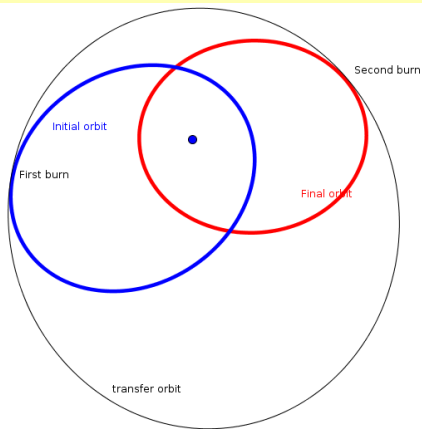
**Step 5:** Calculate velocity of the **target orbit**,  $\vec{v}_{tra}$ , at the point of intersection with **transfer orbit**.

**Step 6:** Calculate the final burn to maneuver into **target orbit**.

$$\Delta \vec{v}_2 = \vec{v}_{tra} - \vec{v}_{tr,2}$$

Step 4 may be easy if you can find the point of intersection,  $\vec{r}_{tr,2}$ , since you can then use the polar equation to find  $f_{tr,2}$ . However, finding the point of intersection may be hard.

# The Choice of Transfer Orbit



## Constraints:

- The **transfer orbit** must intersect both **initial orbit** and **target orbit**
- The  $\Delta v$ 's for entering transfer and orbital insertion are limited by  $\Delta v$  budget
  - ▶ Typically limits us to elliptic transfers.
- There may be constraints on elapsed time.

# Lecture 8

## Spacecraft Dynamics

### The Choice of Transfer Orbit



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The image is of an unproven conjecture that the most efficient 2-burn transfer between 2 coplanar orbits always uses a tangential burn.

- Feel free to find a counterexample!
- Use a brute force search approach using Lambert's problem to calculate  $\Delta v$ 's

# The Choice of Transfer Orbit

Continuity Constraints affect range of  $a$  and  $e$

There are many orbits which intersect both the initial and target orbits.

However, there are some constraints.

Consider

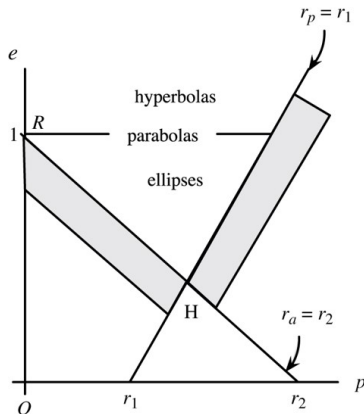
- Circular **initial orbit** of radius  $r_1$
- Circular **target orbit** of radius  $r_2 > r_1$

Obviously, the perigee and apogee of the **transfer orbit** must satisfy

$$r_p = \frac{p}{1+e} \leq r_1$$

and

$$r_a = \frac{p}{1-e} \geq r_2$$



# Lecture 8

## Spacecraft Dynamics

### The Choice of Transfer Orbit

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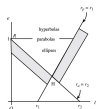
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- The  $r_p$  constraint says the transfer orbit must intersect the initial orbit.
- The  $r_a$  constraint says the transfer orbit must intersect the target orbit.
- The plot illustrates the range of realizable  $p$  and  $e$  for given initial and target radii
- The lines represent

$$p \geq r_2(1 - e) \quad \Leftrightarrow \quad e > 1 - \frac{p}{r_2}$$

and

$$p < r_1(1 + e) \quad \Leftrightarrow \quad e > \frac{p}{r_1} - 1$$

- Again, we assume no constraint on timing or phasing.
- We use  $p$  because it is well-defined for both elliptic and hyperbolic orbits



# Lecture 8

## Spacecraft Dynamics

### Transfer Orbits in Fixed Time

#### Transfer Orbits in Fixed Time

##### Constraints on Transfer Time

Occasionally, we want to arrive at

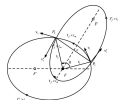
- A certain point in the target orbit,  $r_2^*$
- at a certain time,  $t_f$

Finding the necessary transfer orbit is **Lambert's Problem**.

Primary Applications are:

- Targeting
- Rendez-vous

We will come back to the section on Lambert's problem.



The plot shows 2 possible transfer orbits between point  $P_1$  and  $P_2$ .



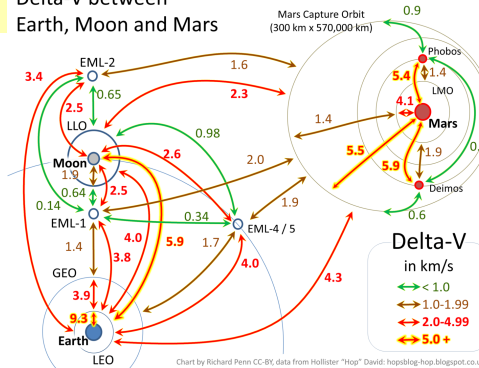
# Constraints on $\Delta v$ budget

What is a minimum energy **transfer orbit**?

The critical resource in space travel is  $\Delta v$ .

- The  $\Delta v$  budget is fixed at takeoff.
- Refueling is not usually possible.
- If you run out of  $\Delta v$ , bad things happen.

## Delta-V between Earth, Moon and Mars



$\Delta v$  can increase or decrease the energy of an orbit.

- The energy difference between 2 orbits must come from somewhere.

$$\Delta E_{\min} = -\frac{\mu}{2a_2} + \frac{\mu}{2a_1}$$

- The closer  $E_{cost}$  is to  $E_{\min}$ , the more efficient the transfer
- $\Delta v$  does not translate directly to Energy changes, however.
- More on this effect later

# Lecture 8

## Spacecraft Dynamics

### Constraints on $\Delta v$ budget

- The energy GAIN for each  $\Delta v$  is actually larger - depending on the initial velocity. We will discuss this more carefully next lecture.
- Note energy is NOT conserved here, so  $\frac{\Delta v^2}{2} \neq \Delta E_{\min}$ .

#### Constraints on $\Delta v$ budget

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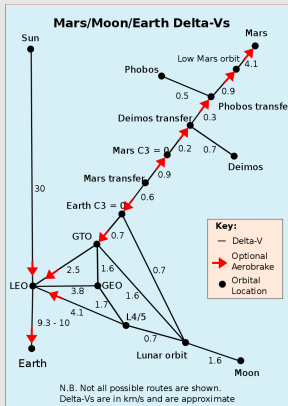
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$$\Delta E_{\text{trans}} = -\frac{\mu}{2a_1} + \frac{\mu}{2a_2}$$

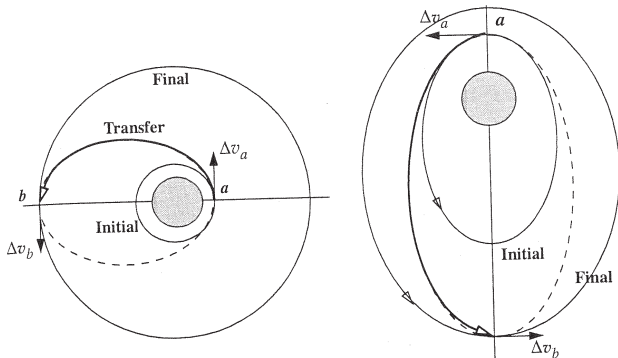
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# The Hohmann Transfer

## A Minimum Energy Orbit?

The Hohmann transfer is the energy-optimal two burn maneuver between any two coaxial elliptic orbits.



- Proposed by Hohmann (1925)
  - ▶ Why?
- Proven for circular target orbits by Lawden (1952)
- Proven for coaxial elliptical initial and target orbits by Thompson (1986)

## Lecture 8

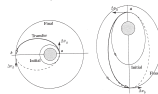
## Spacecraft Dynamics

## The Hohmann Transfer

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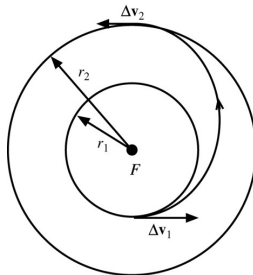
- Also first proposed use of separable lunar landers
- Did not participate in Nazi rocket program.
- Died of hunger/stress after allied bombardment of Essen
- Optimality was originally a conjecture.



- Published in "Die Erreichbarkeit der Himmelskörper (The Attainability of Celestial Bodies)" (1925) [PDF Available Here]

# The Hohmann Transfer

We will first consider the circular case.



## Theorem 3 (The Hohmann Conjecture).

*The  $\Delta v$ -optimal **transfer orbit** between two circular orbits of radii  $r_1$  and  $r_2$  is an elliptic orbit with  $r_p = r_1$  and  $r_a = r_2$*

This yields the orbital elements of the Hohmann **transfer orbit** ( $a, e$ ) as

$$a = \frac{r_a + r_p}{2} = \frac{r_1 + r_2}{2} \quad \text{and} \quad e = 1 - \frac{r_p}{a} = \frac{r_2 - r_1}{r_2 + r_1}$$

# The Hohmann Transfer

To calculate the required  $\Delta v_1$  and  $\Delta v_2$ , the initial velocity is the velocity of a circular orbit of radius  $r_1$

$$v_{init} = \sqrt{\frac{\mu}{r_1}}$$

The required initial velocity is that of the **transfer orbit** at perigee. From the vis-viva equation,

$$v_{trans,p} = \sqrt{\frac{2\mu}{r_1} - \frac{\mu}{a}} = \sqrt{2\mu} \sqrt{\frac{1}{r_1} - \frac{1}{r_1 + r_2}} = \sqrt{2\mu \frac{r_2}{r_1(r_1 + r_2)}}$$

So the initial  $\Delta v_1$  is

$$\Delta v_1 = v_{trans,p} - v_{init} = \sqrt{2\mu \frac{r_2}{r_1(r_1 + r_2)}} - \sqrt{\frac{\mu}{r_1}} = \sqrt{\frac{\mu}{r_1}} \left( \sqrt{\frac{2r_2}{(r_1 + r_2)}} - 1 \right)$$

The velocity of the **transfer orbit** at apogee is

$$v_{trans,a} = \sqrt{\frac{2\mu}{r_2} - \frac{\mu}{a}} = \sqrt{2\mu \frac{r_1}{r_2(r_1 + r_2)}}$$

# The Hohmann Transfer

The required velocity for a circular orbit at apogee is

$$v_{fin} = \sqrt{\frac{\mu}{r_2}}$$

So the final  $\Delta v_2$  is

$$\Delta v_2 = v_{fin} - v_{trans,a} = \sqrt{\frac{\mu}{r_2}} - \sqrt{2\mu \frac{r_1}{r_2(r_1 + r_2)}} = \sqrt{\frac{\mu}{r_2}} \left( 1 - \sqrt{\frac{2r_1}{(r_1 + r_2)}} \right)$$

Thus we conclude to raise a circular orbit from radius  $r_1$  to radius  $r_2$ , we use

$$\Delta v_1 = \sqrt{\frac{\mu}{r_1}} \left( \sqrt{\frac{2r_2}{(r_1 + r_2)}} - 1 \right)$$

$$\Delta v_2 = \sqrt{\frac{\mu}{r_2}} \left( 1 - \sqrt{\frac{2r_1}{(r_1 + r_2)}} \right)$$

# Hohmann Transfer Illustration



# The Hohmann Transfer

## Transfer Time

The Hohmann transfer is optimal

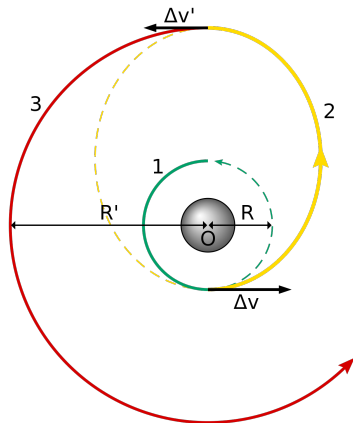
- Only for impulsive transfers
  - ▶ Continuous Thrust is not considered
- Only for **two** impulse transfers
  - ▶ A three impulse transfer can be better
  - ▶ Bi-elliptics are better

The transfer time is simply half the period of the orbit. Hence

$$\begin{aligned}\Delta t &= \frac{\tau}{2} = \pi \sqrt{\frac{a^3}{\mu}} \\ &= \pi \sqrt{\frac{(r_1 + r_2)^3}{8\mu}}\end{aligned}$$

The Hohmann transfer is also the *Maximum Time 2-impulse Transfer*.

- Always a tradeoff between time and efficiency
- Bielliptic Transfers extend this tradeoff.



## Lecture 8

## Spacecraft Dynamics

## The Hohmann Transfer

## The Hohmann Transfer

Transfer Time

The Hohmann transfer is optimal

- Only for impulsive transfers
- Continuous Thrust is not considered
- Only for **two** impulse transfers
- A three impulse transfer can be better
- Bi-elliptics are better

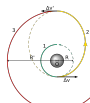
The transfer time is simply half the period of the orbit. Hence

$$\Delta t = \frac{T}{2} = \pi \sqrt{\frac{a^3}{\mu}}$$

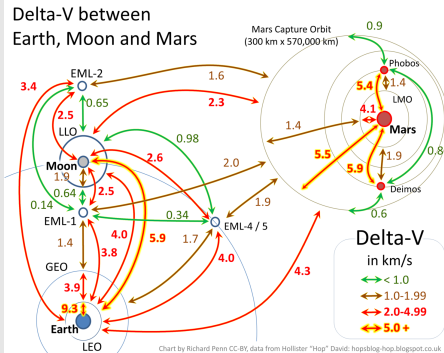
$$= \pi \sqrt{\frac{(r_1 + r_2)^3}{8\mu}}$$

The Hohmann transfer is also the **Maximum Time 2-impulse Transfer**.

- Always a tradeoff between time and efficiency
- Bielliptic Transfers extend this tradeoff.



- The slowest part of the orbit is at apogee.
- Due to Oberth effect, you want to use as much  $\Delta v$  budget as possible at low altitude. Bi-elliptics use this to further reduce  $\Delta v$  at apogee (Next Lecture)
- Hohmann transfer to GEO is extremely wasteful!



# Numerical Example (Parking Orbit to GEO)

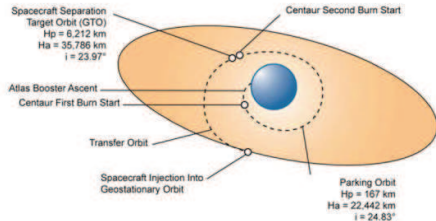
**Problem:** Suppose we are in a circular parking orbit at an altitude of 191.34km and we want to raise our altitude to 35,781km. Describe the required orbital maneuvers (time and  $\Delta v$ ).

**Solution:** We will use a Hohmann transfer between circular orbits of

$$r_1 = 191.35km + 1ER = 1.03ER \quad \text{and} \quad r_2 = 35781km + 1ER = 6.61ER$$

The initial velocity is

$$v_i = \sqrt{\frac{\mu}{r_1}} = .985 \frac{ER}{TU}$$



The transfer ellipse has  $a = \frac{r_1 + r_2}{2} = 3.82ER$ . The velocity at perigee is

$$v_{trans,1} = \sqrt{\frac{2\mu}{r_1} - \frac{\mu}{a}} = 1.296 \frac{ER}{TU}$$

Thus the initial  $\Delta v$  is  $\Delta v_1 = 1.296 - .985 = .315 \frac{ER}{TU}$ .

# Numerical Example

The velocity at apogee is

$$v_{trans,1} = \sqrt{\frac{2\mu}{r_2} - \frac{\mu}{a}} = .202 \frac{ER}{TU}$$

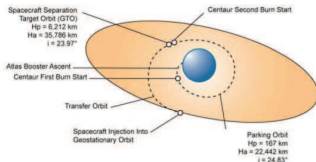
However, the required velocity for a circular orbit at radius  $r_2$  is

$$v_f = \sqrt{\frac{\mu}{r_2}} = .389 \frac{ER}{TU}$$

Thus the final  $\Delta v$  is  $\Delta v_2 = .389 - .202 = .182 \frac{ER}{TU}$ . The second  $\Delta v$  maneuver should be made at time

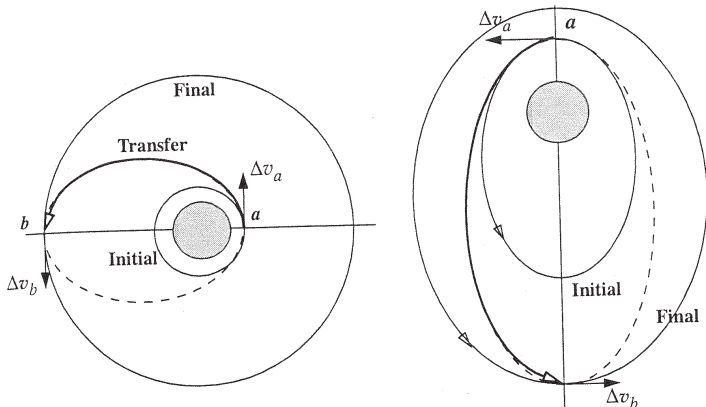
$$t_{fin} = \pi \sqrt{\frac{a^3}{\mu}} = 23.45 TU = 5.256 hr$$

The total  $\Delta v$  budget is  $.497 ER/TU$ .



# The Elliptic Hohmann Transfer

The Hohmann transfer is also energy optimal for coaxial elliptic orbits.



The only ambiguity is whether to make the initial burn at perigee or apogee.

- Need to check both cases
- Often better to make initial burn at perigee
  - ▶ Due to Oberth Effect

# Summary

This Lecture you have learned:

## Coplanar Orbital Maneuvers

- Impulsive Maneuvers
  - ▶  $\Delta v$
- Single Burn Maneuvers
- Hohmann transfers
  - ▶ Elliptic
  - ▶ Circular

**Next Lecture:** Oberth Effect, Bi-elliptics, Out-of-plane maneuvers.