### **Systems Analysis and Control**

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Lecture 23: Drawing The Nyquist Plot

In this Lecture, you will learn:

#### **Review of Nyquist**

#### Drawing the Nyquist Plot

- Using the Bode Plot
- What happens at  $r = \infty$
- Poles on the imaginary axis

#### Phase Margin and Gain Margin

• Reading Stability Margins off the Nyquist Plot

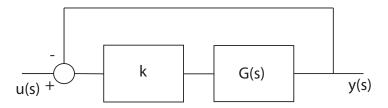
The closed loop is

$$\frac{kG(s)}{1+kG(s)}$$

We want to know when

$$1 + kG(s) = 0$$

**Question:** Does  $\frac{1}{k} + G(s)$  have any zeros in the RHP?



#### Definition 1.

The **Nyquist Contour**,  $C_N$  is a contour which contains the imaginary axis and encloses the right half-place. The Nyquist contour is clockwise.

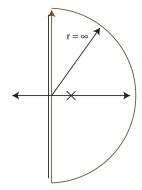
#### A Clockwise Curve

- Starts at the origin.
- Travels along imaginary axis till  $r = \infty$ .
- At  $r = \infty$ , loops around clockwise.
- Returns to the origin along imaginary axis.

We want to know if

$$\frac{1}{k} + G(s)$$

has any zeros in the Nyquist Contour



#### Review

Contour Mapping Principle

**Key Point:** For a point on the mapped contour,  $s^* = G(s)$ ,

 $\angle s^* = \angle G(s)$ 

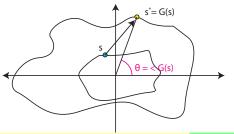
• We measure  $\theta$ , not phase.

To measure the 360° resets in  $\angle G(s)$ 

- We count the number of  $+360^{\circ}$  resets in  $\theta$ !
- We count the number of times  $C_G$  encircles the origin **Clockwise**.

The number of clockwise encirclements of 0 is

• The  $\#_{poles} - \#_{zeros}$  in the RHP

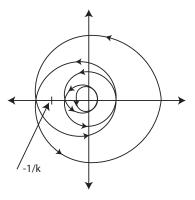


Closed Loop

The number of unstable closed-loop poles is  ${\cal N}+{\cal P},$  where

- N is the number of clockwise encirclements of  $\frac{-1}{k}$ .
- *P* is the number of unstable open-loop poles.

If we get our data from Bode, typically P = 0



How to Plot the Nyquist Curve?

## Plotting the Nyquist Diagram

Example

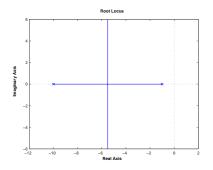
How are we to plot the Nyquist diagram for

$$G(s) = \frac{1}{(\tau_1 s + 1)(\tau_2 s + 1)}$$

• 
$$\tau_1 = 1$$
  
•  $\tau_2 = \frac{1}{10}$ 

First lets take a look at the root locus.

Obviously stable for any k > 0.

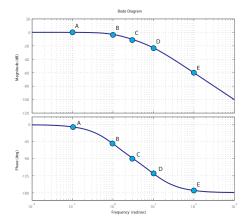


Bode Plot: Lets look at the Frequency Response.

The Bode plot can give us information on  $\left|G\right|$  at different frequencies.

Point	ω	$\angle G$	G
Α	.1	0°	1
В	1	$-45^{\circ}$	.7
С	3	$-90^{\circ}$	.3
D	10	$-135^{\circ}$	.07
E	100	$-175^{\circ}$	.001

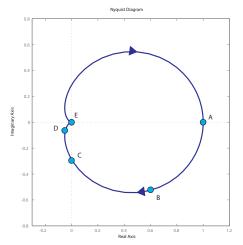
The last two columns give us points on the Nyquist diagram.

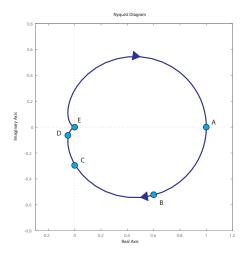


Plot the points from the Bode Diagram.

Point	ω	$\angle G$	G	_
Α	.1	0°	1	-
В	1	$-45^{\circ}$	.7	- We get
С	3	$-90^{\circ}$	.3	- we get
D	10	$-135^{\circ}$	.07	-
E	100	$-175^{\circ}$	.001	-

the upper half of the Nyquist diagram from symmetry.





There are no encirclements of  $-\frac{1}{k}$ .

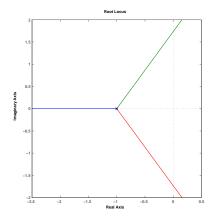
- Stable for all k > 0.
- We already knew that from Root Locus.

#### The Nyquist Plot Example 2

$$G(s) = \frac{1}{(s+1)^3}$$

First lets take a look at the root locus.

We expect instability for large k.

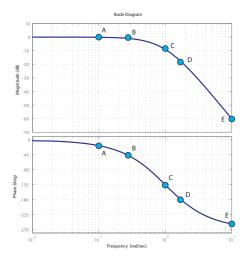


Bode Plot: Lets look at the Frequency Response.

The Bode plot can give us information on |G| at different frequencies.

Point	ω	$\angle G$	G
Α	.1	0°	1
В	.28	$-45^{\circ}$	.95
С	1	$-135^{\circ}$	.35
D	1.8	$-180^{\circ}$	.1
E	10	$-260^{\circ}$	.001

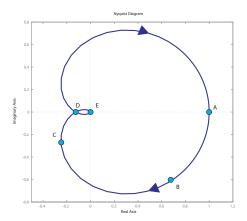
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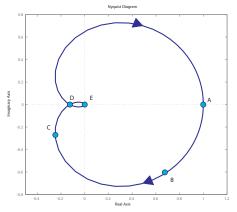


Plot the points from the Bode Diagram.

Point	$\omega$	$\angle G$	G
Α	.1	0°	1
В	.28	$-45^{\circ}$	.95
С	1	$-135^{\circ}$	.35
D	1.8	$-180^{\circ}$	.1
E	10	$-260^{\circ}$	.001

Point D is especially important.





**Point D:** Two CW encirclements when  $-\frac{1}{k} < -.1$  (N=2).

- Instability for  $-\frac{1}{k} < -.1$
- Stable for k < 10.
- Could have used Routh Table.

**Conclusion:** We can use the Bode Plot to map the imaginary axis onto the Nyquist Diagram.

**Question:** What about the other part of the Nyquist contour at  $r = \infty$ ?

Case 1: Strictly Proper.

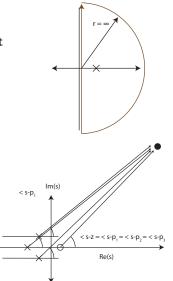
$$\lim_{s \to \infty} |G(s)| = 0$$

What happens at  $\infty$  doesn't matter.

Case 2: Not Strictly Proper.

$$\lim_{s \to \infty} |G(s)| = c$$

Constant Magnitude at  $\infty$ .



Case 2: Not Strictly Proper.

- Angle to all poles and zeros is the same.
- Degree of n(s) and d(s) the same.
  - Number of Poles and Zeros the same.

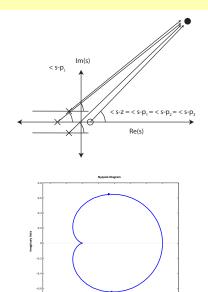
The total angle is

$$\angle G(s) = \sum_{i=1}^{n} \angle (s - z_i) - \sum_{i=1}^{n} \angle (s - p_i)$$
$$= 0$$

The contour map at  $\infty$  has

- Constant magnitude.
- Zero angle.

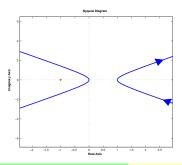
The infinite loop is mapped to a single point! Either (0,0) or (c,0).

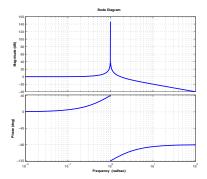


**Another Problem:** Recall the non-inverted pendulum with PD feedback.

$$G(s) = \frac{s+1}{s^2 + \sqrt{\frac{g}{l}}}$$

Magnitude goes to  $\infty$  at  $\omega = \sqrt{\frac{g}{l}}$ . **Question** How do we plot the Nyquist Diagram?



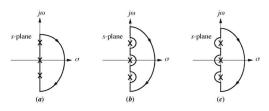


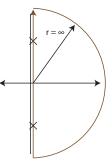
(x,y)

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**Problem:** The Nyquist Contour passes through a pole. Because of the pole, the *argument principle* is invalid.

What to do?





We Modify the Nyquist Contour.

- We detour around the poles.
- Can detour to the right or left.

If we detour to the left, then the poles count as unstable open loop poles.

• P=2

Assume we detour to the right.

• P=0

Look at the detours at small radius.

- Obviously, magnitude  $ightarrow\infty$
- Before the Detour, the phase from the pole is

$$-\angle(s-p) = 90^{\circ}$$

• In the middle of the Detour, the phase from the pole is

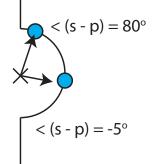
$$-\angle(s-p) = 0^{\circ}$$

• At the end of the Detour, the phase from the pole is

 $-\angle(s-p) = -90^{\circ}$ 

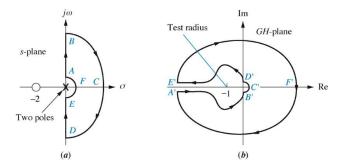
The total phase change through the detour is  $-180^{\circ}$ .

- Corresponds to a CW loop at large radius.
- If there are two or more poles, there is a -180 loop for each pole.



Look at the following example:

$$G(s) = \frac{s+2}{s^2}$$



There are 2 poles at the origin.

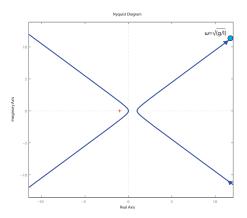
- At  $\omega = 0$ ,
  - $\blacktriangleright \ \angle G(0) = -180^{\circ}$

• 
$$|G(0)| = \infty$$

• 2 poles means  $-360^{\circ}$  loop at  $\omega = 0$ 

#### Lecture 23: Control Systems

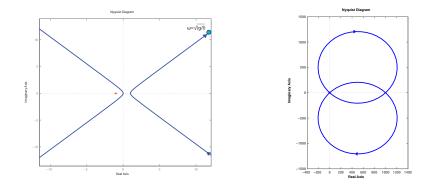
Lets re-examine the pendulum problem with derivative feedback.



Now we can figure out what goes on at  $\infty$ .

• There is a  $-180^{\circ}$  loop at each  $\omega = \sqrt{\frac{g}{l}}$ .

Conclusion: The loops connect in a non-obvious way!



For  $0 < \frac{-1}{k} < 1$ , we have N = 1

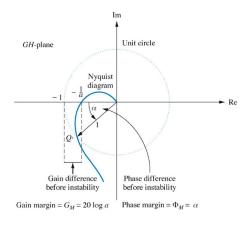
Recall the definitions of Gain Margin.

**Definition 2.** 

The Gain Margin,  $K_m = 1/|G(\imath \omega)|$ when  $\angle G(\imath \omega) = 180^{\circ}$ 

Let  $K_m$  is the maximum stable gain in closed loop.

- $K_m G(s)$  is unstable in closed loop
- Sometimes expressed in dB
- It is easy to find the maximum stable gain from the Nyquist Plot.
  - Find the point  $\frac{-1}{K_m}$  which destabilizes



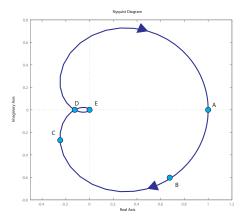
#### Stability Margins Example

#### Recall

$$G(s) = \frac{1}{(s+1)^3}$$

**Stability:** Stable for k < 10.

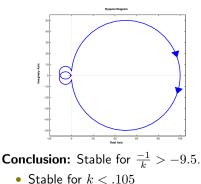
$$K_m = 10$$
 or  $20dB$ .



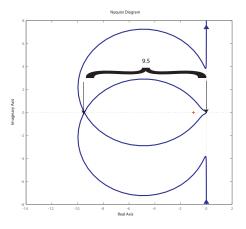
#### Suspension System with integral feedback

There is a pole at the origin.

• CW loop at  $\infty$ .



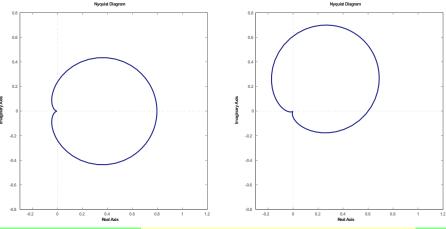
 $K_m = .105$  or -19.5 dB



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Question: What is the effect of a phase change on the Nyquist Diagram.

- A shift in phase changes the angle of all points.
- A Rotation about the origin.
- Will we rotate into instability?

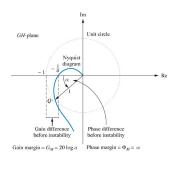


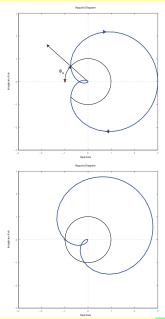
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Recall the definitions of Phase Margin.

#### **Definition 3.**

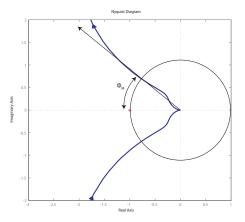
The **Phase Margin**,  $\Phi_M$  is the uniform phase change required to destabilize the system under unitary feedback.





Example

#### **The Suspension Problem**



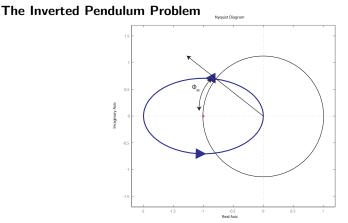
Looking at the intersection with the circle:

• Phase Margin:  $\Phi_M \cong 40^\circ$ 

Gain Margin is infinite.

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Example



Even though open-loop is unstable, we can still find the phase margin:

• Phase Margin:  $\Phi_M \cong 35^{\circ}$ 

Gain Margin is technically undefined because open loop is unstable.

• There is a minimum gain, not a maximum.

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Lecture 23: Control Systems

What have we learned today?

#### **Review of Nyquist**

#### Drawing the Nyquist Plot

- Using the Bode Plot
- What happens at  $r=\infty$
- Poles on the imaginary axis

#### Phase Margin and Gain Margin

• Reading Stability Margins off the Nyquist Plot

#### Next Lecture: Controller Design in the Frequency Domain